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Citation: Han, Lei, Cheng, Xuefeng, Jiang, Lei, Li, Rong, Ding, Guofu and Qin, Sheng-feng (2017) Research on parametric modeling and grinding methods of bottom edge of toroid-shaped end-milling cutter. Proceedings of the Institution of Mechanical Engineers, Part B: Journal of Engineering Manufacture. ISSN 0954-4054 (In Press)

Published by: SAGE Publications

URL: <https://doi.org/10.1177/0954405417717547>  
<<https://doi.org/10.1177/0954405417717547>>

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# **Research on parametric modeling and grinding methods of bottom edge of toroid-shaped end milling cutter**

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## **Abstract**

For a toroid-shaped end milling cutter to have multi-structure features of tooth offset center and introversion of bottom edge, this paper proposes a generalized parametric modeling method of the bottom edge, including a straight edge segment and a circular arc edge segment. And based on the parametric model this paper also deduces the corresponding tool path for grinding of the bottom edge's rake and flank faces. The parametric modeling method is based on the geometric analytic equations while the grinding method is driven by the proposed parametric model and the parameters of rake and flank faces. The two methods can be applied to a bottom edge of a cutter with multi-structure features to guarantee  $G^1$  continuity at the two joints for connecting a circular arc edge with a straight edge and a conical helix edge respectively. In order to verify the accuracy of proposed methods, experiments were carried out. The modeling and grinding experimental results verified the accuracy and utility of the methods.

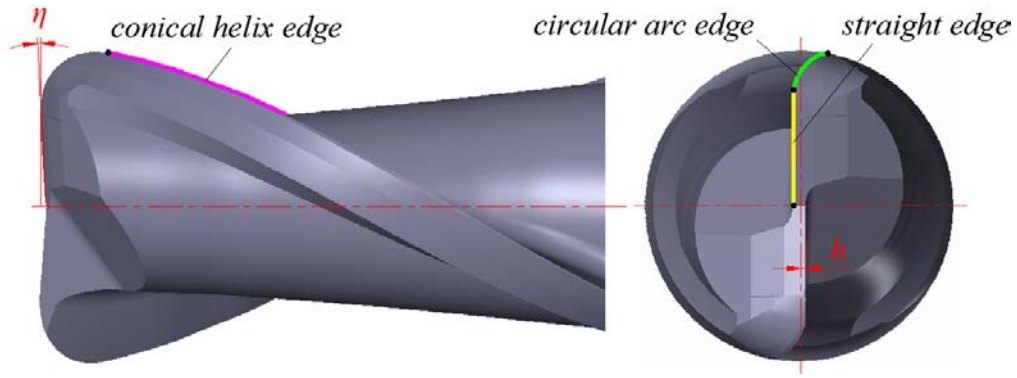
## **Key words**

Toroid-shaped end milling cutter; bottom edge; parametric modeling method; grinding method; integrated tool design and manufacturing

## 1 Introduction

Toroid-shaped end milling cutter (TEMC) is widely used in manufacturing of complicated parts with free-form surfaces<sup>[1]</sup>. The main parts of cutting edges participated in milling are a straight edge, a circular arc edge and a conical helix edge shown in Fig. 1. TEMC has the advantages of high adaptability and machining efficiency compared with ball-end milling cutter under constant scallop-height cutting<sup>[2]</sup>. And it has the ability to produce the periphery of parts meeting with the bottom floor with fillets<sup>[3]</sup>. Also, this type of cutter has higher material removal rate and lower flank wear rate because bottom edge is more solid<sup>[4][5]</sup> and thus, the machining quality is much more stable<sup>[6]</sup> compared with flat-end milling cutter.

Generally, the straight edge on TEMC having a tooth offset to the bottom center can improve its strength, and introversion to reduce friction between bottom edge and machined surface. As shown in Fig. 1,  $h$  is the tooth offset distance and  $\eta$  is the dish angle. Meanwhile TEMC has smooth cutting edges to ensure the cutting continuity during machining. However, the multi-structure features lead to difficulties in parametric modeling and grinding. Although there is a complete set of theory that can be used to design and manufacture TEMC without multi-structure features at present, it cannot be applied directly to TEMC with multi-structure features. Therefore the research on parametric modeling and grinding methods of this kind of TEMC is of great significance.



**Fig. 1** Main parts of cutting edges (Straight edge has multi-structure features)

Precise parametric modeling of a bottom edge which determines the structure of end milling cutter is an essential for grinding of TEMC. Furthermore, the edge curve is also the guideline of the grinding wheel movement during grinding. Therefore parametric modeling of a bottom edge must be studied first. Many scholars have done much research about it. Chen adopted a supplementary cutting edge with a constant pitch to supply a general reference for TEMC with a constant angle between the cutting edge and the cutter axis<sup>[6]</sup>. Chen presented a precise mathematical modeling procedure for the design of cutters with a circular arc edge, the cutting edge forms a constant angle with the longitude curve<sup>[7]</sup>, and presented a systematically design model of the involute end-milling cutter which cutting edge curves forms a constant angle with the cutter axis<sup>[8]</sup>. Chen presented a design model of TEMC, the cutting edge forms an approximately constant angle with the cutter axis<sup>[9]</sup>. Lin proposed a geometrical model of the cutting edge on TEMC with a constant angle between the cutting edge and the cutter axis<sup>[10]</sup>. Hsieh derived a mathematical model of the ideal conical helix edge which formed a constant angle to the longitudinal line at the toroid surface<sup>[11]</sup>. Tang studied the design models of the cutting edge with the convex curve generatrix, and put forward three mathematical models, i.e., planar cutting edges, helical cutting edges with a constant angle to the meridian and helical cutting edges with a constant pitch to avoid the problem of the inexistence of the cutting edge in the area near the end face of a cutter and the cutting edges are smoothly connected<sup>[12][13]</sup>. Yang introduced the design of a cutting edge with equal pitch, and the edge was continuous at the joint of the circular torus and the cylindrical surface<sup>[14]</sup>. Han gave the design method of the cutting edge which was defined as an approximate equal

pitch curve with a concave arc as generator<sup>[15]</sup>. Lv established a mathematic model using infinitesimal geometry for the cutting edge design which used equal lead helix<sup>[16][17]</sup>. Although references [1], [18] and [19] used the generalized mathematical model proposed by Engin and Altintas<sup>[3][20][21]</sup>, and seven geometric parameters were defined, if the circular torus is not a full quarter, there will be a discontinuity on the bottom edge. Cheng used the orthogonal helix edge curve as the S-shaped edge curve of ball-end milling cutter, the edge curve acquired based on the mathematical model proposed has a good S-shape and can connect with the circumferential edge curve smoothly. Furthermore, the model can be used easily to establish the S-shaped edge curve with tooth offset center or without tooth offset center<sup>[22]</sup>.

Until now, several kinds of curves are used as a bottom edge on TEMC, such as an equal pitch edge curve, an equal helix angle edge curve with the longitude line, an equal helix angle edge curve with the cutter axis, a planar edge curve and an orthogonal helix edge curve. They have good edge curve shapes and can be used in series types of TEMC. However, present modeling methods using these kinds of curves are not concerned with a straight edge, not to mention the straight edge with multi-structure features, thus leading to complexity and difficulty of the grinding method. The grinding methods of TEMC are also studied by many scholars. Liu proposed a grinding process of the rake and flank faces and calculated the tool path and direction vector of grinding wheel<sup>[4]</sup>. Chen obtained the sectional profile of the grinding wheel by using an inverse problem-solving technique and the manufacturing model presented can be used on a two-axis NC machine<sup>[7]</sup>. Lin provided grinding models of a section design, feeding speeds and relative position of the grinding wheel<sup>[10]</sup>. Hsieh developed a systematic method for the grinding of the helical flute and the cutting edge, and considered the section profile and relative feeding velocities of the grinding wheel<sup>[11]</sup>. Bao studied a virtual two-axis grinding model of TEMC with an equal helix lead cutting edge and an equal helix angle cutting edge respectively<sup>[23]</sup>.

In the above studies, many scholars focused on the parametric modeling and grinding methods of TEMC without multi-structure features of tooth offset to the

center and introversion of the bottom edge. And thus the existing research results are just in a limited scope of application of the methods presented and no unified model is formed. In order to meet the requirements of the design and manufacturing of a toroid-shaped end milling cutter especially its bottom edge has multi-structure features, this article presents a generalized parametric modeling method of a bottom edge, and based on this, a grinding method for the rake and flank faces of the bottom edge can make the cutting edges with  $G^1$  continuity, that is (1) the cutting edge curves meet at the joint points and (2) their tangent directions at the joints are the same. The  $G^1$  continuity makes the composite cutting edge smooth. The modeling and grinding experiments indicates that the proposed cutter modelling and grinding methods can shorten the production cycle and improve the success rate of the design of a toroid-shaped end milling cutter, thus reduce the cost of cutter production. Furthermore, the proposed general and parametric modelling of a TEMC has a great potential to support optimal cutter design for different machining applications and the corresponding grinding method can easily realize the cutter design into tool manufacturing. This provides an integrated cutting design and manufacturing solution for wider applications.

This article is organized as follows: Section 2 describes the mathematical model of a bottom edge with multi-structure features of tooth offset center and introversion. Section 3 presents a grinding method of a bottom edge based on its 3D mathematical model. The experiments and results are described in section 4, and finally conclusions are drawn in section 5.

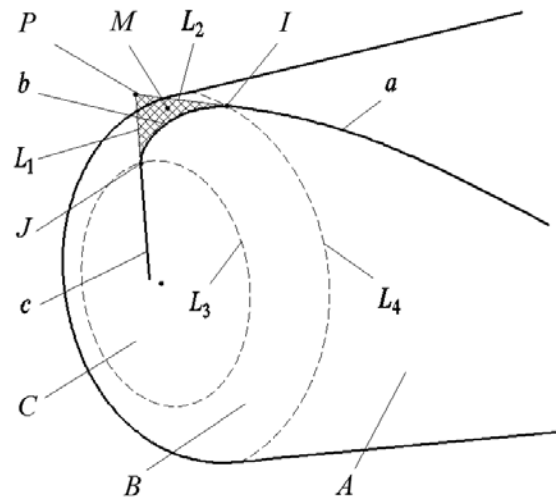
## **2 Parametric modeling method of bottom edge**

Among many kinds of curves mentioned above, the planar edge curve has a good curve shape and more simple mathematical computation compared with others. This type of edge curve can reach  $G^1$  continuity at the two joints of a circular arc edge with a straight edge and a conical helix edge respectively, and the straight edge can have

multi-structure features whether or not. So planar edge curve is adopted, i.e., the circular arc edge is the intersecting planar curve of the circular torus and the plane composed of an extended line of straight edge and a tangential line at the end of the conical helix edge.

As shown in Fig. 2, the revolving surfaces of the cutting edges on TEMC are defined as three parts: a circular truncated conical surface  $A$  where the conical helix edge  $a$  lies, a circular torus  $B$  where the circular arc edge  $b$  lies, and a concave conical surface  $C$ . Their relationship is that  $B$  is tangent with  $A$  and  $C$ . Straight edge  $c$  has the multi-structure features of tooth offset center and introversion.

Define  $I$  as the intersection of  $a$  and  $b$ ,  $J$  as the intersection of  $b$  and  $c$ . Define  $L_1$  as the extended line of  $c$ ,  $L_2$  as the tangential line of  $a$  at  $I$ ,  $L_3$  as the intersecting line of  $B$  and  $C$ ,  $L_4$  as the intersecting line of  $A$  and  $B$ . Define  $P$  as the intersection of  $L_1$  and  $L_2$ . Plane  $M$  is composed of  $L_1$  and  $L_2$ . The bottom edge consists of  $b$  and  $c$ .



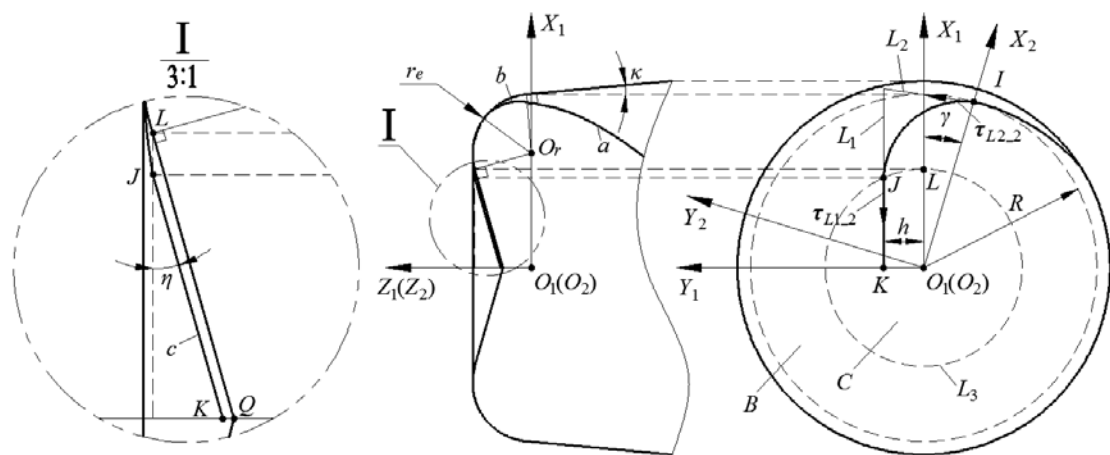
**Fig. 2** Relevant geometrical elements of bottom edge

## 2.1 Parametric model of edge $c$

To reduce the complexity of mathematical modeling, define the coordinate system  $[O_1-X_1Y_1Z_1]$  as the first coordinate system, and the origin  $O_1$  as center of  $B$ .  $Z_1$  is the cutter axis and the positive direction is from the cutter shank to the tip.  $X_1$  is parallel to the projection of  $c$  on the plane  $X_1Y_1$ . The point coordinates in the first coordinate system are identified by subscript  $_1$ .

Let  $\gamma$  be the angle between  $X_1$ -axis and the projection of  $IO_1$  on the plane  $X_1Y_1$ . Rotate the first coordinate system on  $Z_1$ -axis by angle  $\gamma$  negatively, and the coordinate system  $[O_2-X_2Y_2Z_2]$  is obtained as the second coordinate system. The point coordinates in the second coordinate system are identified by subscript  $_2$ . Then, the parametric models of  $c$  and  $b$  can be described in the second coordinate system.

As shown in Fig. 3, define  $L$  as the intersection of  $L_3$  and the plane  $X_1Z_1$ ,  $Q$  as the tip of  $C$ ,  $K$  as the endpoint of  $c$ ,  $O_r$  as the center of the cross section of  $B$  on the plane  $X_1Z_1$ . Let  $r_e$  be the section radius of  $B$ ,  $R$  be the distance between  $I$  and the cutter axis,  $\kappa$  be the half cone angle of  $A$ ,  $\beta$  be the helix angle of  $a$  at  $I$  (angle between the helix edge on the revolving surface and the generator curve).



**Fig. 3** Schematic diagram for the design of edge  $c$

On the basis of cutter geometry relationship, the coordinates of  $J$  and  $K$  in the first coordinate system are as follows

$$\mathbf{J}_{-1} = \begin{bmatrix} x_{J-1} \\ y_{J-1} \\ z_{J-1} \end{bmatrix} = \begin{bmatrix} \sqrt{(x_{Or-1} - r_e \cdot \sin \eta)^2 - h^2} \\ h \\ r_e \cdot \cos \eta \end{bmatrix}, \quad (1)$$

$$\mathbf{K}_{-1} = \begin{bmatrix} x_{K-1} \\ y_{K-1} \\ z_{K-1} \end{bmatrix} = \begin{bmatrix} 0 \\ h \\ r_e \cdot \cos \eta - \sqrt{(x_{Or-1} - r_e \cdot \sin \eta)^2 - h^2} \tan \eta \end{bmatrix}. \quad (2)$$

According to the direction of the coordinate system, the rotation transformation matrix from the first coordinate system to the second coordinate system can be



expressed as follows

$$\mathbf{T}_{1\_2} = \begin{bmatrix} \cos \gamma & \sin \gamma & 0 \\ -\sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{bmatrix}. \quad (3)$$

Obviously, the coordinates of  $I$  can be described as

$$\mathbf{I}_{\_2} = \begin{bmatrix} x_{I\_2} \\ y_{I\_2} \\ z_{I\_2} \end{bmatrix} = \begin{bmatrix} R \\ 0 \\ r_e \cdot \sin \kappa \end{bmatrix}, \quad (4)$$

where:  $R = x_{Or\_1} + r_e \cdot \cos \kappa$ .

Let  $\boldsymbol{\tau}_{L1\_2}$ ,  $\boldsymbol{\tau}_{L2\_2}$  be the unit direction vector of  $L_1$  and  $L_2$  respectively. Then  $\boldsymbol{\tau}_{L1\_2}$  and the parametric equation  $L_{1\_2}(t_1)$  of  $L_1$  can be obtained by Eqs. (5) and (6) respectively

$$\boldsymbol{\tau}_{L1\_2} = \begin{bmatrix} \tau_{L1x\_2} \\ \tau_{L1y\_2} \\ \tau_{L1z\_2} \end{bmatrix} = \begin{bmatrix} -\cos \gamma \cdot \cos \eta \\ -\sin \gamma \cdot \cos \eta \\ -\sin \eta \end{bmatrix}, \quad (5)$$

$$L_{1\_2}(t_1) = \begin{cases} x = x_{J\_2} + t_1 \cdot \tau_{L1x\_2}, \\ y = y_{J\_2} + t_1 \cdot \tau_{L1y\_2}, \\ z = z_{J\_2} + t_1 \cdot \tau_{L1z\_2}. \end{cases} \quad (6)$$

where  $t_1$  is the independent variable.

Similarly,  $\boldsymbol{\tau}_{L2\_2}$  and the parametric equation  $L_{2\_2}(t_2)$  of  $L_2$  can be obtained by Eqs. (7) and (8) respectively

$$\boldsymbol{\tau}_{L2\_2} = \begin{bmatrix} \tau_{L2x\_2} \\ \tau_{L2y\_2} \\ \tau_{L2z\_2} \end{bmatrix} = \begin{bmatrix} -\cos \beta \cdot \sin \kappa \\ \sin \beta \\ \cos \beta \cdot \cos \kappa \end{bmatrix}, \quad (7)$$

$$L_{2\_2}(t_2) = \begin{cases} x = x_{I\_2} + t_2 \cdot \tau_{L2x\_2}, \\ y = y_{I\_2} + t_2 \cdot \tau_{L2y\_2}, \\ z = z_{I\_2} + t_2 \cdot \tau_{L2z\_2}. \end{cases} \quad (8)$$

where  $t_2$  is the independent variable.

For  $L_1$  and  $L_2$  intersect at  $P$ , then

$$\begin{cases} x_{P_{-2}} = x_{J_{-2}} + t_1 \cdot \tau_{L1x_{-2}} = x_{I_{-2}} + t_2 \cdot \tau_{L2x_{-2}} \\ y_{P_{-2}} = y_{J_{-2}} + t_1 \cdot \tau_{L1y_{-2}} = y_{I_{-2}} + t_2 \cdot \tau_{L2y_{-2}} \cdot \\ z_{P_{-2}} = z_{J_{-2}} + t_1 \cdot \tau_{L1z_{-2}} = z_{I_{-2}} + t_2 \cdot \tau_{L2z_{-2}} \end{cases} \quad (9)$$

So  $t_1$ ,  $t_2$  and  $\gamma$  can be obtained by Eqs. (5) to (9), shown as follows

$$\begin{cases} \sin \gamma = \frac{(y_{I_{-2}} + t_2 \cdot \tau_{L2y_{-2}})(x_{J_{-1}} - t_1 \cdot \cos \eta) - (x_{I_{-2}} + t_2 \cdot \tau_{L2x_{-2}})y_{J_{-1}}}{y_{J_{-1}}^2 + (x_{J_{-1}} - t_1 \cdot \cos \eta)^2}, \\ \cos \gamma = \frac{(x_{I_{-2}} + t_2 \cdot \tau_{L2x_{-2}})(x_{J_{-1}} - t_1 \cdot \cos \eta) + (y_{I_{-2}} + t_2 \cdot \tau_{L2y_{-2}})y_{J_{-1}}}{y_{J_{-1}}^2 + (x_{J_{-1}} - t_1 \cdot \cos \eta)^2}, \end{cases} \quad (10)$$

where:  $t_1 = \frac{-T_2 + \sqrt{T_2^2 - 4T_1 \cdot T_3}}{2T_1};$

$$t_2 = \frac{z_{J_{-1}} - z_{I_{-2}} - t_1 \cdot \sin \eta}{\tau_{L2z_{-2}}};$$

$$T_1 = (\tau_{L2x_{-2}}^2 + \tau_{L2y_{-2}}^2) \sin^2 \eta - \tau_{L2z_{-2}}^2 \cdot \cos^2 \eta;$$

$$T_2 = 2 \left\{ x_{J_{-1}} \cdot \tau_{L2z_{-2}}^2 \cdot \cos \eta - \left[ \tau_{L2x_{-2}} (x_{I_{-2}} \cdot \tau_{L2z_{-2}} - z_{I_{-2}} \cdot \tau_{L2x_{-2}} + z_{J_{-1}} \cdot \tau_{L2x_{-2}}) + \right. \right. \\ \left. \left. \tau_{L2y_{-2}} (y_{I_{-2}} \cdot \tau_{L2z_{-2}} - z_{I_{-2}} \cdot \tau_{L2y_{-2}} + z_{J_{-1}} \cdot \tau_{L2y_{-2}}) \right] \sin \eta \right\};$$

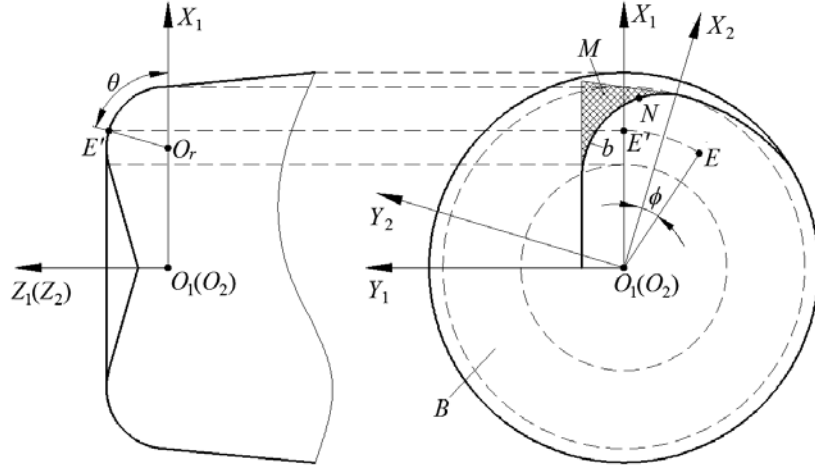
$$T_3 = (x_{I_{-2}} \cdot \tau_{L2z_{-2}} - z_{I_{-2}} \cdot \tau_{L2x_{-2}} + z_{J_{-1}} \cdot \tau_{L2x_{-2}})^2 + \\ (y_{I_{-2}} \cdot \tau_{L2z_{-2}} - z_{I_{-2}} \cdot \tau_{L2y_{-2}} + z_{J_{-1}} \cdot \tau_{L2y_{-2}})^2 - (x_{J_{-1}}^2 + y_{J_{-1}}^2) \tau_{L2z_{-2}}^2.$$

For  $c$  and  $L_1$  are collinear, the unit direction vector  $\tau_{c_{-2}}$  and parametric equation  $c_{-2}(t_1)$  of edge  $c$  can be obtained by Eqs. (5) and (6) respectively, and the range of  $t_1$  is  $[0, |x_{J_{-2}}/\tau_{L1x_{-2}}|]$ .

## 2.2 Parametric model of edge $b$

As shown in Fig. 4, define  $E$  as an arbitrary point on  $B$ ,  $E'$  as the rotating projection of  $E$  on the plane  $X_1Z_1$ ,  $N$  as an arbitrary point on bottom edge. Let  $\theta$  be the angle between  $E'O_r$  and  $X_1$ -axis (counter clockwise direction is positive),  $\phi$  be the angle between the projection of  $EO_2$  on the plane  $X_2Y_2$  and  $X_2$ -axis (clockwise

direction is positive).



**Fig. 4** Schematic diagram for the design of edge  $b$

The normal vector  $\mathbf{n}_{M-2}$  of  $M$  is determined by the vector cross-product of  $\boldsymbol{\tau}_{L1-2}$  and  $\boldsymbol{\tau}_{L2-2}$  as follows

$$\mathbf{n}_{M-2} = \begin{bmatrix} n_{Mx-2} \\ n_{My-2} \\ n_{Mz-2} \end{bmatrix} = \boldsymbol{\tau}_{L1-2} \times \boldsymbol{\tau}_{L2-2} = \begin{bmatrix} \sin \beta \cdot \sin \eta - \cos \beta \cdot \cos \kappa \cdot \cos \eta \cdot \sin \gamma \\ \cos \beta \cdot \cos \kappa \cdot \cos \eta \cdot \cos \gamma + \cos \beta \cdot \sin \kappa \cdot \sin \eta \\ -\cos \beta \cdot \sin \kappa \cdot \cos \eta \cdot \sin \gamma - \sin \beta \cdot \cos \eta \cdot \cos \gamma \end{bmatrix}, \quad (11)$$

Hence, the equation of  $M$  can be obtained by Eq. (12)

$$n_{Mx-2}(x - x_{I-2}) + n_{My-2}(y - y_{I-2}) + n_{Mz-2}(z - z_{I-2}) = 0. \quad (12)$$

By the definition of the circular torus<sup>[26]</sup>, the parametric equation of  $B$  can be written as

$$B_{-2}(\theta, \phi) = \begin{cases} x = (x_{Or-1} + r_e \cdot \cos \theta) \cos \phi, \\ y = (x_{Or-1} + r_e \cdot \cos \theta) \sin \phi, \\ z = r_e \cdot \sin \theta, \end{cases} \quad \left( \kappa \leq \theta \leq \frac{\pi}{2} + \eta, 0 \leq \phi < 2\pi \right). \quad (13)$$

Since  $b$  is defined as a planar curve, then  $b$  is the intersecting line of  $M$  and  $B$  and angle  $\phi$  can be determined by Eqs. (12) and (13)

$$\begin{cases} \sin \phi = \frac{n_{My-2}(T_4 - n_{Mz-2} \cdot r_e \cdot \sin \theta) - n_{Mx-2} \sqrt{(n_{Mx-2}^2 + n_{My-2}^2)(x_{Or-1} + r_e \cdot \cos \theta)^2 - (T_4 - n_{Mz-2} \cdot r_e \cdot \sin \theta)^2}}{(n_{Mx-2}^2 + n_{My-2}^2)(x_{Or-1} + r_e \cdot \cos \theta)}, \\ \cos \phi = \frac{n_{Mx-2}(T_4 - n_{Mz-2} \cdot r_e \cdot \sin \theta) + n_{My-2} \sqrt{(n_{Mx-2}^2 + n_{My-2}^2)(x_{Or-1} + r_e \cdot \cos \theta)^2 - (T_4 - n_{Mz-2} \cdot r_e \cdot \sin \theta)^2}}{(n_{Mx-2}^2 + n_{My-2}^2)(x_{Or-1} + r_e \cdot \cos \theta)}, \end{cases} \quad (14)$$

where:  $T_4 = x_{I_{-2}} \cdot n_{Mx_{-2}} + y_{I_{-2}} \cdot n_{My_{-2}} + z_{I_{-2}} \cdot n_{Mz_{-2}}$ .

Substituting Eq. (14) into Eq. (13) gives the parametric equation  $b_{-2}(\theta)$  of edge  $b$

$$b_{-2}(\theta) = \begin{cases} x = \frac{n_{Mx_{-2}}(T_4 - n_{Mz_{-2}} \cdot r_e \cdot \sin \theta) + n_{My_{-2}} \sqrt{(n_{Mx_{-2}}^2 + n_{My_{-2}}^2)(x_{Or_{-1}} + r_e \cdot \cos \theta)^2 - (T_4 - n_{Mz_{-2}} \cdot r_e \cdot \sin \theta)^2}}{(n_{Mx_{-2}}^2 + n_{My_{-2}}^2)}, \\ y = \frac{n_{My_{-2}}(T_4 - n_{Mz_{-2}} \cdot r_e \cdot \sin \theta) - n_{Mx_{-2}} \sqrt{(n_{Mx_{-2}}^2 + n_{My_{-2}}^2)(x_{Or_{-1}} + r_e \cdot \cos \theta)^2 - (T_4 - n_{Mz_{-2}} \cdot r_e \cdot \sin \theta)^2}}{(n_{Mx_{-2}}^2 + n_{My_{-2}}^2)}, \quad \left( \kappa \leq \theta \leq \frac{\pi}{2} + \eta \right), \\ z = r_e \cdot \sin \theta, \end{cases} \quad (15)$$

Take the derivative of Eq. (15) with respect to  $\theta$ , the unit direction vector  $\tau_{b_{-2}}(\theta)$  of edge  $b$  can be expressed as

$$\tau_{b_{-2}}(\theta) = \begin{bmatrix} \tau_{bx_{-2}} \\ \tau_{by_{-2}} \\ \tau_{bz_{-2}} \end{bmatrix} = \begin{bmatrix} \frac{-n_{My_{-2}} \cdot T_6 \cdot T_7 \cdot \sin \theta + n_{My_{-2}} \cdot n_{Mz_{-2}} \cdot T_5 \cdot \cos \theta - n_{Mx_{-2}} \cdot n_{Mz_{-2}} \sqrt{T_6 \cdot T_7^2 - T_5^2} \cos \theta}{T_6 \sqrt{T_6 \cdot T_7^2 - T_5^2} + (T_5 \cdot \sin \theta - T_7 \cdot n_{Mz_{-2}} \cdot \cos \theta)^2} \\ \frac{n_{Mx_{-2}} \cdot T_6 \cdot T_7 \cdot \sin \theta - n_{Mx_{-2}} \cdot n_{Mz_{-2}} \cdot T_5 \cdot \cos \theta - n_{My_{-2}} \cdot n_{Mz_{-2}} \sqrt{T_6 \cdot T_7^2 - T_5^2} \cos \theta}{T_6 \sqrt{T_6 \cdot T_7^2 - T_5^2} + (T_5 \cdot \sin \theta - T_7 \cdot n_{Mz_{-2}} \cdot \cos \theta)^2} \\ \frac{\sqrt{T_6 \cdot T_7^2 - T_5^2} \cos \theta}{\sqrt{T_6 \cdot T_7^2 - T_5^2} + (T_5 \cdot \sin \theta - T_7 \cdot n_{Mz_{-2}} \cdot \cos \theta)^2} \end{bmatrix}, \quad \left( \kappa \leq \theta \leq \frac{\pi}{2} + \eta \right), \quad (16)$$

where:  $T_5 = T_4 - n_{Mz_{-2}} \cdot r_e \cdot \sin \theta$ ;

$$T_6 = n_{Mx_{-2}}^2 + n_{My_{-2}}^2;$$

$$T_7 = x_{Or_{-2}} + r_e \cdot \cos \theta.$$

### 2.3 The generalized helix angle of edge $b$

The parametric model of edge  $b$  is already obtained. Although edge  $b$  is a planar edge curve, it can be also regarded as a curve with a variable helix angle. At present, the generalized helix angle on the revolving surface has two definitions<sup>[24]</sup>: one is the angle between the helix edge on the revolving surface and the generator curve<sup>[22]</sup>, the other is the angle between the helix edge on the revolving surface and the cutter axis<sup>[25]</sup>. The first definition is considered in this paper. The unit tangent vector of the generator curve of  $B$  at  $E$  can be expressed in the following form

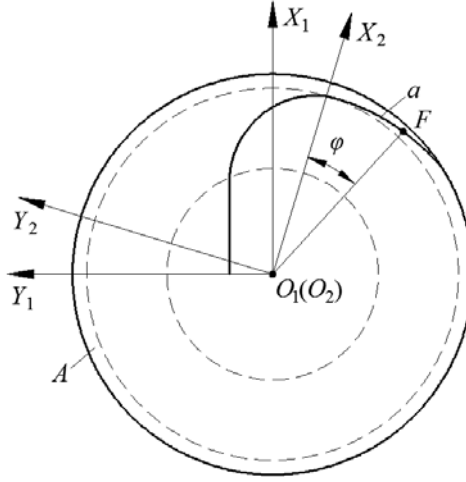
$$\boldsymbol{\tau}_{BE_{-2}}(\theta) = \begin{bmatrix} -\sin \theta \cos \phi \\ \sin \theta \sin \phi \\ \cos \theta \end{bmatrix} \quad (17)$$

Hence the generalized helix angle at  $N$  can be given by

$$\begin{aligned} \beta_r &= \arccos \frac{\boldsymbol{\tau}_{BE_{-2}}(\theta) \cdot \boldsymbol{\tau}_{b_{-2}}(\theta)}{|\boldsymbol{\tau}_{BE_{-2}}(\theta)| \cdot |\boldsymbol{\tau}_{b_{-2}}(\theta)|} \\ &= \arccos \frac{\sqrt{T_6 \cdot T_7^2 - T_5^2}}{\sqrt{T_6 \cdot T_7^2 - T_5^2 + (T_5 \cdot \sin \theta - T_7 \cdot n_{Mz_{-2}} \cdot \cos \theta)^2}}, \quad \left( \kappa \leq \theta \leq \frac{\pi}{2} + \eta \right). \end{aligned} \quad (18)$$

## 2.4 Parametric model of edge $a$

As shown in Fig. 5, define  $F$  as an arbitrary point on  $a$ . Let  $\varphi$  be the angle between the projection of  $FO_2$  on the plane  $X_2Y_2$  and  $X_2$ -axis (clockwise direction is positive).



**Fig. 5** Schematic diagram for the design of edge  $a$

By the definition of the generalized helix, the parametric equation  $a_2(\varphi)$  of edge  $a$  can be written as

$$a_{-2}(\varphi) = \begin{cases} x = x_{I_{-2}} \cdot e^{-\varphi \cdot \sin(-\kappa) \cdot \cot \beta} \cdot \cos \varphi, \\ y = -x_{I_{-2}} \cdot e^{-\varphi \cdot \sin(-\kappa) \cdot \cot \beta} \cdot \sin \varphi, \\ z = -\frac{x_{I_{-2}} [1 - e^{-\varphi \cdot \sin(-\kappa) \cdot \cot \beta}]}{\tan(-\kappa)} + r_e \cdot \sin \kappa, \end{cases} \quad (\varphi \geq 0). \quad (19)$$

Take the derivative of Eq. (19) with respect to  $\varphi$ , the unit direction vector  $\tau_{a_{-2}}(\varphi)$  of edge  $a$  can be expressed as

$$\tau_{a_{-2}}(\varphi) = \begin{bmatrix} \tau_{ax_{-2}} \\ \tau_{ay_{-2}} \\ \tau_{az_{-2}} \end{bmatrix} = \begin{cases} x = \frac{T_8}{\sqrt{T_8^2 + T_9^2 + T_{10}^2}}, \\ y = \frac{T_9}{\sqrt{T_8^2 + T_9^2 + T_{10}^2}}, \\ z = \frac{T_{10}}{\sqrt{T_8^2 + T_9^2 + T_{10}^2}}, \end{cases} \quad (\varphi \geq 0). \quad (20)$$

where:  $T_8 = -\sin \kappa \cdot \cot \beta \cdot \cos \varphi + \sin \varphi$  ;

$T_9 = \sin \kappa \cdot \cot \beta \cdot \sin \varphi + \cos \varphi$  ;

$T_{10} = \cos \kappa \cdot \cot \beta$  .

### 3 Grinding method of bottom edge

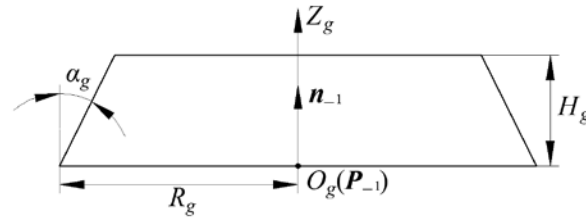
Parametric model of the bottom edge is the base of the tool path of the grinding wheel. Bottom edge is the intersection curve of rake face and flank face, and its structural parameters are guaranteed by the grinding process of the two faces. For TEMC has a complex structure and lots of parameters and the purpose of the grinding method in this paper is to guarantee the precision of parameters related to bottom edge, the detailed method of the section profile formation was not presented here for simplification purpose. For convenience, the tool path calculation is deduced in the first coordinate system thus the origin of programming is  $O_1$  and grinding wheel wear

is not considered.

### 3.1 Parameters of the grinding wheel

The profile of V-shaped grinding wheel and Cup-shaped grinding wheel can both be defined by three parameters. Let  $R_g$  (the radius of the big-end of the grinding wheel),  $H_g$  (the thickness of the grinding wheel) and  $\alpha_g$  (the taper angle of the grinding wheel) be three given geometric parameters of the grinding wheel profile, shown in Fig. 6.

Define the coordinate system  $[O_g-X_gY_gZ_g]$  as the grinding wheel coordinate system, and the origin  $O_g$  as the center of the big-end of the grinding wheel,  $Z_g$  as the grinding wheel axis. Let  $\mathbf{n}_{-1}$  (the unit direction vector of  $Z_g$ -axis) and  $\mathbf{P}_{-1}$  (the coordinates of the origin  $O_g$ ) be two parameters of tool path in the first coordinate system. Define  $\nu$  as the inclined angle in grinding process. Let  $\nu$  be  $\nu'$  in rake face grinding and let  $\nu$  be  $\nu''$  in flank face grinding.



**Fig. 6** Geometric parameters of the profile of grinding wheel

### 3.2 Grinding tool path for rake face

The grinding of the rake face of bottom edge is to form the chip-breaker-groove of the end cutting edge and the normal rake angle of TEMC.

Define the coordinate system  $[O_n-X_nY_nZ_n]$  as the movable normal-section local coordinate system, the origin  $O_n$  coincides with  $N$ ,  $Z_n$ -axis is tangent to the bottom edge and  $X_n$ -axis and the cutter axis lies in the same plane. In the grinding process,  $\nu'$  (the inclined angle restrained by the depth of chip-breaker-groove in rake face grinding) and  $\gamma_n$  (the normal rake angle of bottom edge) are pre-designed.

In a rake face grinding process, the coordinate system  $[O'_g-X'_gY'_gZ'_g]$  can be

obtained from the coordinate system  $[O_n-X_nY_nZ_n]$  by the following steps: rotate the coordinate system  $[O_n-X_nY_nZ_n]$  around  $Z_n$ -axis by angle  $\gamma_n$  positively, then around  $Y_n$ -axis by angle  $\nu'$  negatively, around  $X_n$ -axis by  $90^\circ$  negatively, at last translate the rotated coordinate system from  $O_n$  to  $O'_g$  to get the grinding wheel coordinate system.

Let  $\mathbf{N}_{-1}=[x_{N-1}, y_{N-1}, z_{N-1}]^T$  be the coordinates of  $N$  in the first coordinate system. Define  $\mathbf{T}_{1-n}$  and  $\mathbf{R}_{1-n}$  as translation and rotation homogeneous transformation matrix(HTM) from the coordinate system  $[O_1-X_1Y_1Z_1]$  to  $[O_n-X_nY_nZ_n]$  respectively,  $\mathbf{T}'_{n-g}$  and  $\mathbf{R}'_{n-g}$  as translation and rotation HTM from the coordinate system  $[O_n-X_nY_nZ_n]$  to  $[O'_g-X'_gY'_gZ'_g]$  in rake face grinding process respectively as shown in Fig. 7. They can be obtained by Eqs. (19) to (22)

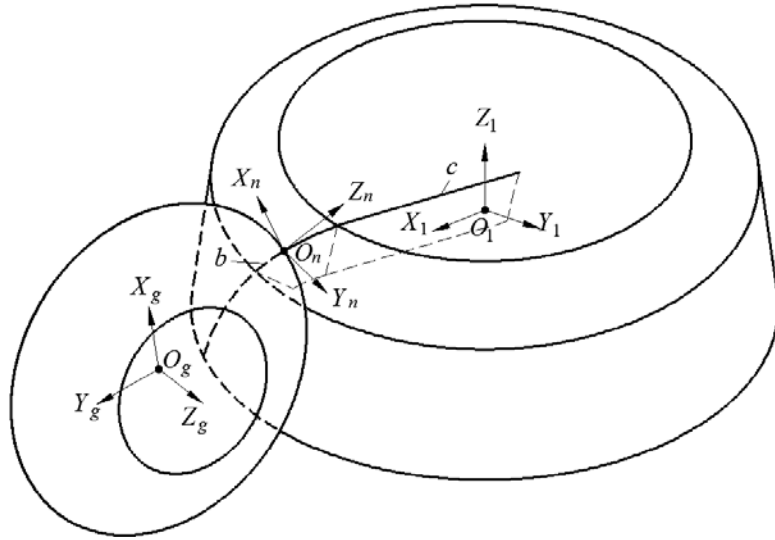
$$\mathbf{T}_{1-n} = \begin{bmatrix} 1 & 0 & 0 & x_{N-1} \\ 0 & 1 & 0 & y_{N-1} \\ 0 & 0 & 1 & z_{N-1} \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (21)$$

$$\mathbf{R}_{1-n} = \begin{bmatrix} \cos \theta & 0 & -\sin \theta & 0 \\ 0 & 1 & 0 & 0 \\ \sin \theta & 0 & \cos \theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \beta_r & \sin \beta_r & 0 \\ 0 & -\sin \beta_r & \cos \beta_r & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \left( \kappa \leq \theta \leq \frac{\pi}{2} + \eta \right) \quad (22)$$

$$\mathbf{T}'_{n-g} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & R_g \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (23)$$

$$\mathbf{R}'_{n-g} = \begin{bmatrix} \cos \gamma_n & -\sin \gamma_n & 0 & 0 \\ \sin \gamma_n & \cos \gamma_n & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \nu_1 & 0 & -\sin \nu_1 & 0 \\ 0 & 1 & 0 & 0 \\ \sin \nu_1 & 0 & \cos \nu_1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (24)$$





**Fig. 7** Schematic diagram for rake face grinding

- (1) The vector of the grinding wheel axis

According to the HTM theory, the vector of the grinding wheel axis in rake face grinding can be expressed as follows

$$\mathbf{n}'_{-1} = \mathbf{R}_{1-n} \mathbf{R}'_{n-g} [0 \ 0 \ 1 \ 0]^T \quad (25)$$

- (2) The position of CL point

According to the HTM theory, the position of CL point in rake face grinding can be expressed in the following form

$$\mathbf{P}'_{-1} = \mathbf{T}_{1-n} \mathbf{R}_{1-n} \mathbf{R}'_{n-g} \mathbf{T}'_{n-g} [0 \ 0 \ 0 \ 1]^T \quad (26)$$

### 3.3 Grinding tool path for flank face

The grinding of the flank face of bottom edge is to form the normal relief angle of TEMC.

In the grinding process,  $\nu''$  (the inclined angle to avoid interference between grinding wheel and other tooth in flank face grinding) and  $\alpha_n$  (the normal relief angle of bottom edge) are pre-designed.

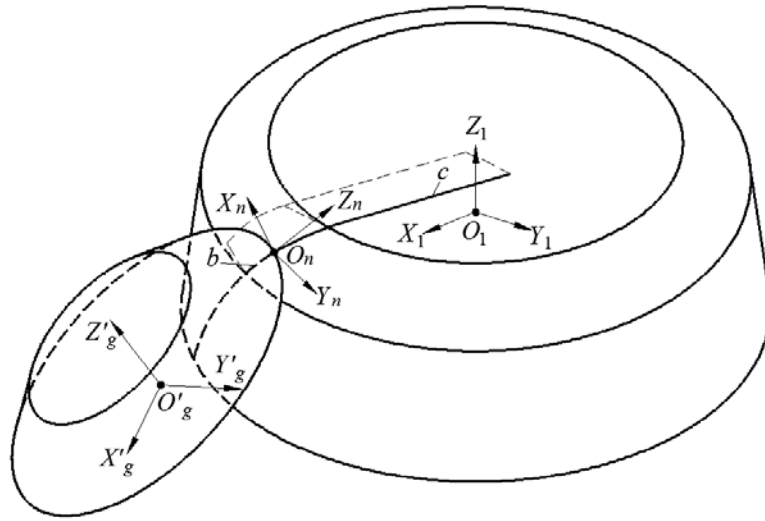
In a flank face grinding process, the coordinate system  $[O''_g-X''_g-Y''_g-Z''_g]$  can be obtained from the coordinate system  $[O_n-X_n-Y_n-Z_n]$  by the following steps: rotate the coordinate system  $[O_n-X_n-Y_n-Z_n]$  around  $Z_n$ -axis by angle  $\alpha_n$  negatively, then around

$X_n$ -axis by angle  $\nu''$  positively, around  $Y_n$ -axis by  $90^\circ$  negatively, at last translate the rotated coordinate system from  $O_n$  to  $O''_g$  to get the grinding wheel coordinate system for flank face grinding.

Define  $T''_{n-g}$  and  $R''_{n-g}$  as translation and rotation HTM from coordinate system  $[O_n-X_nY_nZ_n]$  to  $[O''_g-X''_gY''_gZ''_g]$  in flank face grinding process respectively as shown in Fig. 8. They can be obtained by Eqs. (25) and (26)

$$T''_{n-g} = \begin{bmatrix} 1 & 0 & 0 & R_{g2} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (27)$$

$$R''_{n-g} = \begin{bmatrix} \cos \alpha_n & \sin \alpha_n & 0 & 0 \\ -\sin \alpha_n & \cos \alpha_n & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \nu_2 & -\sin \nu_2 & 0 \\ 0 & \sin \nu_2 & \cos \nu_2 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (28)$$



**Fig. 8** Schematic diagram for flank face grinding

- (1) The vector of the grinding wheel axis

According to the HTM theory, the vector of the grinding wheel axis in flank face grinding can be expressed as follows

$$\mathbf{n}''_{-1} = \mathbf{R}_{l-n} \mathbf{R}''_{n-g} [0 \ 0 \ 1 \ 0]^T \quad (29)$$

- (2) The position of CL point

According to the HTM theory, the position of CL point in flank face grinding can be expressed in the following form

$$\mathbf{P}''_{-1} = \mathbf{T}_{1-n} \mathbf{R}_{1-n} \mathbf{R}''_{n-g} \mathbf{T}''_{n-g} \begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix}^T \quad (30)$$

## 4 Experiments and results

### 4.1 Modeling experiment

To verify the validity of the proposed parametric modeling method, modeling experiment was carried out in MATLAB. To validate the  $G^1$  continuity at the two joints of a circular arc edge with the connected straight edge and conical helix edge, one TEMC with multi-structure features of tooth offset center and introversion of its straight edge was taken for example. The design values related to parametric modeling of the cutting edge are shown in Table 1.

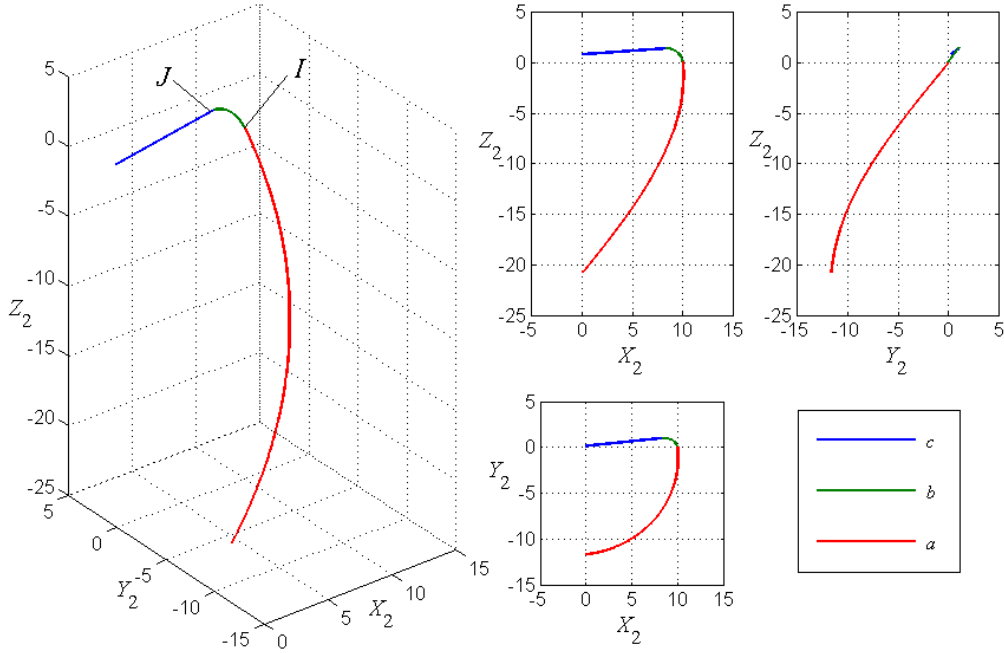
**Table 1** Design values related to parametric modeling of the cutting edge

Parameters	$2R$ (mm)	$r_e$ (mm)	$h$ (mm)	$\eta$ (°)	$\kappa$ (°)	$\beta$ (°)
Design values	20	1.5	0.2	4	4.5	39

The calculated coordinates of  $J$  on  $c$  by substituting  $t_1=0$  into Eq. (6) is set as  $\mathbf{J}_{2c}$ . The calculated coordinates of  $J$  on  $b$  by substituting  $\theta=\pi/2+\eta$  into Eq. (15) is set as  $\mathbf{J}_{2b}$ . The calculated coordinates of  $I$  on  $b$  by substituting  $\theta=\kappa$  into Eq. (15) is set as  $\mathbf{I}_{2b}$ . The calculated coordinates of  $I$  on  $a$  by substituting  $\varphi=0$  into Eq. (19) is set as  $\mathbf{I}_{2a}$ . The calculated unit tangential vector of  $c$  at  $J$  by Eq. (5) is set as  $\boldsymbol{\tau}_{J2c}$ . The calculated unit tangential vector of  $b$  at  $J$  by substituting  $\theta=\pi/2+\eta$  into Eq. (16) is set as  $\boldsymbol{\tau}_{J2b}$ . The calculated unit tangential vector of  $b$  at  $I$  by substituting  $\theta=\kappa$  into Eq. (16) is set as  $\boldsymbol{\tau}_{I2b}$ . The calculated unit tangential vector of  $a$  at  $I$  by substituting  $\varphi=0$  into Eq. (20) is set as  $\boldsymbol{\tau}_{I2a}$ . The modeling parameters of one tooth are shown in Table 2 and the result in MATLAB is shown in Fig. 9.

**Table 2** Modeling parameters

Equations	Conditions	Parameters	Calculated values
Eq. (6)	$t_1=0$	$\mathbf{J}_{2c}$ (mm)	$[8.3341, 1.0504, 1.4963]^T$
Eq. (15)	$\theta=\pi/2+\eta$	$\mathbf{J}_{2b}$ (mm)	$[8.3341, 1.0504, 1.4963]^T$
Eq. (15)	$\theta=\kappa$	$\mathbf{I}_{2b}$ (mm)	$[10.0000, 0.0000, 0.1177]^T$
Eq. (19)	$\varphi=0$	$\mathbf{I}_{2a}$ (mm)	$[10.0000, 0.0000, 0.1177]^T$
Eq. (5)	\	$\boldsymbol{\tau}_{J_{2c}}$	$[-0.9924, -0.1014, -0.0698]^T$
Eq. (16)	$\theta=\pi/2+\eta$	$\boldsymbol{\tau}_{J_{2b}}$	$[-0.9924, -0.1014, -0.0697]^T$
Eq. (16)	$\theta=\kappa$	$\boldsymbol{\tau}_{I_{2b}}$	$[-0.0610, 0.6293, 0.7748]^T$
Eq. (20)	$\varphi=0$	$\boldsymbol{\tau}_{I_{2a}}$	$[-0.0610, 0.6293, 0.7748]^T$



**Fig. 9** Modeling result of the bottom edge and the conical helix edge in MATLAB

The calculated and modeling results validate the  $G^1$  continuity at the two joints and prove the accuracy of the parametric modeling method.

## 4.2 Grinding experiment

The machining accuracy of the grinding tool path was verified by the grinding experiment. The parameters of the grinding wheel profile and grinding process are shown in Table 3. The allowable absolute errors of machining are  $0.1\text{mm}/0.5^\circ$ .

**Table 3** Parameters of the grinding wheel profile and grinding process

Grinding process	Parameters of grinding wheel					
	Shape	Type	$R_g$ (mm)	$H_g$ (mm)	$\alpha_g$ (°)	$\nu$ (°)
Rake face grinding	V-shape	12V9	50	25	45	75
Flank face grinding	Cup-shape	11V9	50	32	30	60

Based on the mathematical models of TEMC, the grinding tool path in grinding of the tested TEMC was calculated by the grinding method put forward. Part of the grinding tool path file obtained by the grinding method put forward is shown below

“.....

GOTO/34.687784, -1.083085, -3.482481, -0.089849, 0.769583, -0.632194  
GOTO/34.688929, -1.095449, -3.472860, -0.089220, 0.769622, -0.632236  
GOTO/34.690062, -1.107808, -3.463239, -0.088592, 0.769661, -0.632276  
GOTO/34.691183, -1.120164, -3.453619, -0.087964, 0.769700, -0.632316  
GOTO/34.692292, -1.132515, -3.444000, -0.087335, 0.769740, -0.632355  
GOTO/34.693389, -1.144862, -3.434381, -0.086707, 0.769780, -0.632393  
GOTO/34.694474, -1.157205, -3.424763, -0.086079, 0.769820, -0.632430  
GOTO/34.695548, -1.169544, -3.415145, -0.085450, 0.769860, -0.632466  
GOTO/34.696610, -1.181879, -3.405528, -0.084822, 0.769901, -0.632502  
GOTO/34.697659, -1.194210, -3.395911, -0.084194, 0.769941, -0.632536  
GOTO/34.698697, -1.206536, -3.386296, -0.083566, 0.769982, -0.632570

.....”

The NC codes were generated by post-process from the grinding tool path and were verified in a grinding process. The material of TEMC was cemented carbide. The trial product grinded by ANCA FastGrind CNC cutter grinding machine tool is shown in Fig. 10.



**Fig. 10** Trial product of TEMC

(1) Measurement of the major parameters

The major parameters of the trial product were measured by Zoller genius-3 tool measuring instrument using the principle of non-contact light perception scanning in no vibration environment and at room temperature. In the “ELEPHANT” module of the instrument, choose the parameters which require measurement and then the instrument can automatically measure the parameters within the accuracy of 0.001mm/0.01°. Measured the values three times over all different parameters and took the average as the final measured values to reduce measurement errors. The major design values and the corresponding trial product measured values are shown in Table 4.

**Table 4** Comparison of major design and measured values

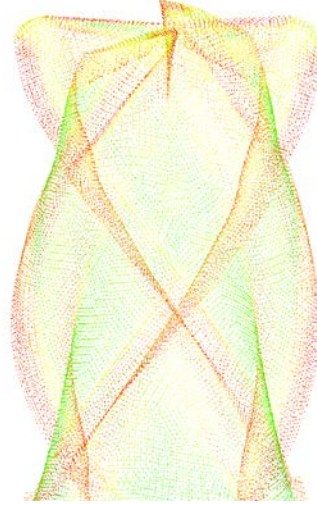
Parameters	$2R$ (mm)	$r_e$ (mm)	$h$ (mm)	$\eta$ (°)	$\gamma_n$ (°)	$\alpha_n$ (°)
Major design values	20	1.5	0.2	4	8	14
Trial product measured values	19.991	1.483	0.215	4.23	8.31	13.73

(2) Measurement of the bottom edge

The point cloud of the trial product was measured and obtained by Solutionix Rexcan III 3D optical scanner within the accuracy of 0.007mm. The 3D optical scanning and the point cloud of the trial product are shown in Fig. 11.



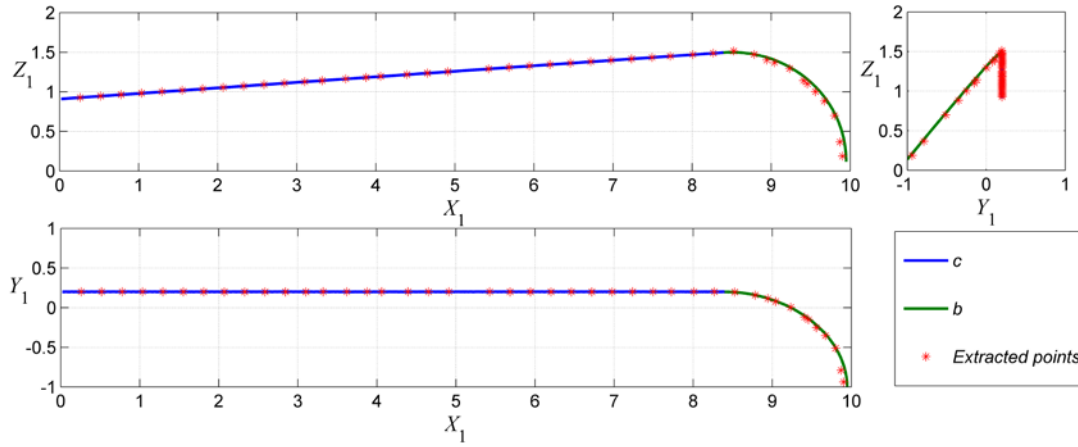
(a) 3D optical scanning



(b) Point cloud

**Fig. 11** 3D optical scanning and point cloud of the trial product

In total, 31 points on edge  $c$  and 12 points on edge  $b$  were extracted from the point cloud (see Fig.11). The extracted points and the theoretical bottom edge are built up in MATLAB as shown in Fig. 12.



**Fig. 12** The theoretical bottom edge and the extracted points

The coordinates of the extracted points were obtained and the distances between the extracted points and the theoretical bottom edge were calculated. The maximum distances for edge  $c$  and  $b$  are 0.021mm and 0.055mm separately.

According to the measurement results of the major parameters on the bottom edge, the maximum absolute errors of the trial product grinded by the proposed grinding method are 0.055mm/0.31°. And they are both within the allowable tolerance range. The precision of the major parameters and the edge position meets the requirement of machining, and the effectiveness of the tool path for grinding of the

rake and flank faces of bottom edge is illustrated.

## **5 Conclusions**

In this study, a generalized and accurate parametric modeling method and the corresponding grinding methods of a bottom edge of TEMC are presented. The bottom edge acquired based on this parametric modeling method can possess multi-structure features of tooth offset center or introversion. Furthermore, the parametric equations of the bottom edge are put forward, and the bottom edge can meet  $G^1$  continuity at the two joints of a circular arc edge with a straight edge and a conical helix edge, respectively. The grinding method is driven by the parametric model of the bottom edge and the design values of its rake and flank faces. And it can realize the accurate calculation of the tool path for grinding. Finally, the utility and accuracy of the parametric modeling and grinding methods are verified through a series of experiments.

It is believed that the proposed general and parametric modelling of the cutting edges of a TEMC with multi-features can be used to optimize cutter design for different application scenarios by setting up a proper set of parameters. Upon achieving the optimal cutter design, its corresponding grinding method is also ready to be applied effectively in the cutter (tool) manufacturing. Therefore, the integration of the cutter design modelling and the associated grinding method provide an integral solution for optimal cutter design and manufacturing.

## **Acknowledgement**

This work is supported by the Special Fund of High-end CNC Machine Tools and Basic Manufacturing Equipment (2015ZX04001002), China.



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## Appendix

### Notation

$a$	conical helix edge
$a_2(\varphi)$	parametric equation of edge $a$ in the second coordinate system
$A$	circular truncated conical surface
$b$	circular arc edge
$b_2(\theta)$	parametric equation of edge $b$ in the second coordinate system
$B$	circular torus
$B_2(\theta, \phi)$	parametric equation of $B$ in the second coordinate system
$c$	Straight edge
$c_2(t_1)$	parametric equation of edge $c$ in the second coordinate system

$C$	concave conical surface
$E$	an arbitrary point on $B$
$E'$	rotating projection of $E$ on the plane $X_1Z_1$
$h$	distance of tooth offset the center
$H_g$	thickness of the grinding wheel
$I$	intersection of $a$ and $b$
$I_{-2}$	coordinates of $I$ in the second coordinate system
$I_{-2a}$	calculated coordinates of $I$ on $a$ by substituting $\varphi=0$ into Eq. (19)
$I_{-2b}$	calculated coordinates of $I$ on $b$ by substituting $\theta=\kappa$ into Eq. (15)
$J$	intersection of $b$ and $c$
$J_{-1}$	coordinates of $J$ in the first coordinate system
$J_{-2}$	coordinates of $J$ in the second coordinate system
$J_{-2b}$	calculated coordinates of $J$ on $b$ by substituting $\theta=\pi/2+\eta$ into Eq. (15)
$J_{-2c}$	calculated coordinates of $J$ on $c$ by substituting $t_1=0$ into Eq. (6)
$K$	endpoint of $c$
$K_{-1}$	coordinates of $K$ in the first coordinate system
$L$	intersection of $L_3$ and the plane $X_1Z_1$
$L_1$	extended line of $c$
$L_{1-2}(t_1)$	parametric equation of $L_1$ in the second coordinate system
$L_2$	tangential line of $a$ at $I$
$L_{2-2}(t_2)$	parametric equation of $L_2$ in the second coordinate system
$L_3$	intersecting line of $B$ and $C$
$L_4$	intersecting line of $A$ and $B$
$M$	plane composed of $L_1$ and $L_2$
$N$	arbitrary point on bottom edge
$n_{-1}$	unit direction vector of axis $Z_g$ in the first coordinate system
$n'_{-1}$	vector of the grinding wheel axis in rake face grinding in the first coordinate system
$n''_{-1}$	vector of the grinding wheel axis in flank face grinding in the first coordinate system

	system
$\mathbf{n}_{M\_2}$	normal vector of $M$ in the second coordinate system
$N$	an arbitrary point on bottom edge
$N\_1$	coordinates of $N$ in the first coordinate system
$O_g$	center of the big-end of the grinding wheel
$O_r$	center of the cross section of $B$ on the plane $X_1Z_1$
$[O_1-X_1Y_1Z_1]$	first coordinate system
$[O_2-X_2Y_2Z_2]$	second coordinate system
$[O_g-X_gY_gZ_g]$	grinding wheel coordinate system
$[O'_g-X'_gY'_gZ'_g]$	grinding wheel coordinate system in rake face grinding
$[O''_g-X''_gY''_gZ''_g]$	grinding wheel coordinate system in flank face grinding
$[O_n-X_nY_nZ_n]$	normal-section local coordinate system
$P$	intersection of $L_1$ and $L_2$
$P\_1$	coordinates of the origin $O_g$ in the first coordinate system
$P'\_1$	position of CL point in rake face grinding in the first coordinate system
$P''\_1$	position of CL point in flank face grinding in the first coordinate system
$Q$	tip of $C$
$r_e$	section radius of $B$
$R$	distance between $I$ and the cutter axis
$\mathbf{R}_{1-n}$	rotation HTM from coordinate system $[O_1-X_1Y_1Z_1]$ to $[O_n-X_nY_nZ_n]$
$R_g$	radius of the big-end of the grinding wheel
$\mathbf{R}'_{n-g}$	rotation HTM from coordinate system $[O_n-X_nY_nZ_n]$ to $[O'_g-X'_gY'_gZ'_g]$
$\mathbf{R}''_{n-g}$	rotation HTM from coordinate system $[O_n-X_nY_nZ_n]$ to $[O''_g-X''_gY''_gZ''_g]$
$T_{1-2}$	translation HTM from the first coordinate system to the second coordinate system
$T_{1-n}$	translation HTM from coordinate system $[O_1-X_1Y_1Z_1]$ to $[O_n-X_nY_nZ_n]$
$T'_{n-g}$	translation HTM from coordinate system $[O_n-X_nY_nZ_n]$ to $[O'_g-X'_gY'_gZ'_g]$
$T''_{n-g}$	translation HTM from coordinate system $[O_n-X_nY_nZ_n]$ to $[O''_g-X''_gY''_gZ''_g]$
$\alpha_g$	taper angle of the grinding wheel

$\alpha_n$	normal relief angle of bottom edge
$\beta$	helix angle of $a$ at $I$
$\beta_r$	generalized helix angle at $N$
$\gamma$	angle between the positive direction of $X_1$ and $X_2$
$\gamma_n$	normal rake angle of bottom edge
$\eta$	dish angle
$\theta$	angle between $E'O_r$ and $X_1$ -axis
$\kappa$	half cone angle of $A$
$\nu$	the inclined angle in grinding process
$\nu'$	the inclined angle in rake face grinding
$\nu''$	the inclined angle in flank face grinding
$\tau_{a\_2}(\varphi)$	unit direction vector of edge $a$ in the second coordinate system
$\tau_{b\_2}(\theta)$	unit direction vector of edge $b$ in the second coordinate system
$\tau_{BE\_2}(\theta)$	unit tangent vector of the generator curve of $B$ at $E$ in the second coordinate system
$\tau_{c\_2}$	unit direction vector of edge $c$ in the second coordinate system
$\tau_{I\_2a}$	calculated unit tangential vector of $a$ at $I$ by substituting $\varphi=0$ into Eq. (20)
$\tau_{I\_2b}$	calculated unit tangential vector of $b$ at $I$ by substituting $\theta=\kappa$ into Eq. (16)
$\tau_{J\_2b}$	calculated unit tangential vector of $b$ at $J$ by substituting $\theta=\pi/2+\eta$ into Eq. (16)
$\tau_{J\_2c}$	calculated unit tangential vector of $c$ at $J$ by Eq. (5)
$\tau_{L1\_2}$	unit direction vector of $L_1$ in the second coordinate system
$\tau_{L2\_2}$	unit direction vector of $L_2$ in the second coordinate system
$\varphi$	angle between the projection of $FO_2$ on the plane $X_2Y_2$ and $X_2$ -axis
$\phi$	angle between the projection of $EO_2$ on the plane $X_2Y_2$ and $X_2$ -axis